



Fabrication of Pebax/4A Zeolite Nanocomposite Membrane to Enhance CO₂ Selectivity Compared to Pure O₂, N₂, and CH₄ Gases

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ABSTRACT

The separation of carbon dioxide is essential for the environment. Using membranes to separate this gas is economical, but the weakness in permeability and mechanical strength has prevented their commercialization. Robeson proved that permeability and selectivity have the opposite relationship and provided an upper limit for pairs of gases. Worth to be mentioned that any membrane placed above this limit could be commercialized. Scientists proposed mixed matrix membranes to overcome this problem. These membranes contain two phases, polymer, and inorganic. This research focused on membrane technology and aimed to prepare a membrane that has a good performance for CO₂ separation and at the same time its cost is economical, so by adding a reasonable price zeolite available in the market named 4A to the Pebax 1657 polymer and changing the operating conditions of the process, permeability and Selectivity was measured. Pebax polymer and 4A zeolite were selected as respectively the polymer and mineral phases for membrane fabrication. The fabricated membranes were evaluated by XRD, FT-IR, FE-SEM, BET, EDAX, TGA/DSC, and mechanical strength tests. Finally, the selectivity of CO₂ compared to N₂, O₂, and CH₄ improved by 53, 67, and 75%, respectively, and obtained a good position on the Robeson diagram.

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NOMENCLATURE

<i>XRD</i>	X-ray diffraction	<i>a, BET</i>	Specific surface area based on BET analysis (m ² g ⁻¹)
<i>FT-IR</i>	Infrared Fourier transforms	<i>L</i>	Membrane thickness (cm)
<i>FE-SEM</i>	Field emission scanning electron microscopy	<i>V</i>	Tank volume after the membrane (cm ³)
<i>BET</i>	Brunauer-Emmett-Teller	<i>P_o</i>	Absolute input gas pressure (psia)
<i>EDAX</i>	X-ray energy scattering spectroscopy	<i>A</i>	Membrane area (cm ²)
<i>TGA</i>	Thermal balance analysis	<i>V_m</i>	Monolayer volume (cm ³ (STP) g ⁻¹)
<i>TPV</i>	Total pore volume (cm ³ g ⁻¹)	% <i>Wt.</i>	Weight percent
<i>P_A</i>	Gas permeability A (Barrer)	<i>g</i>	Mass unit in grams
<i>α_{A/B}</i>	The selectivity of A over B	<i>DMF</i>	Dimethylformamide solvent
<i>μm</i>	Micro metr (10 ⁻⁶ m)	<i>dP/dt</i>	Pressure changes in time (bar/s)

1. INTRODUCTION

The separation of carbon dioxide from the exhaust gases of chemical industries to preserve the environment and comply with standards has become an essential issue for industrial managers. When is not considered high purity in the separation of gases, membrane separation is the

best technique [1,2]. The process of membrane separation requires small amount of energy [3-5].

Recently, researchers have for gases separation used Polyphosphazene, Polyamides, Cellulose acetate, Polyether-urethane, Polyamide-polyether-block copolymers, and Poly-vinylidene fluoride [2].

Lin et al. [6] concluded that using polar groups in polymers leads to a high selectivity for carbon dioxide

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compared to light gases. Copolymers containing ethylene oxides, such as polyether-block-amide or Pebax, are a very suitable proposal to achieve this aim [6]. Pebax is an elastomeric thermoplastic with a chemical structure as illustrated in Figure 1.

PA is an aliphatic polyamide that forms the hard part and PE polyether forms the soft part. The PA block provides mechanical resistance, and the passage of gas occurs from the PE phase. This polymer has good mechanical, and thermal stability [7].

Permeability and selectivity are two crucial actors in gas separation. Robeson reported a comprehensive analysis of gas pair permeability in polymer membranes. He proved that there is an inverse relationship between permeability and selectivity. In other words, these two factors have an opposite relationship [8]. Scientists are looking for a solution that increases permeability and selectivity simultaneously. One of their solutions is making composite membranes. These types of membranes include the polymer phase and filler phase [9-11]. With a combination of properties favorable to polymer membranes (high selectivity) and fillers (permeability and high mechanical stability), a stable and adjustable structure can be created, therewith expanding gas separation technology.

PEBA polymers provide the opportunity to produce membranes at a low cost. these polymers are commercially produced and can be converted into films with low thickness and excellent quality. The penetration, absorption, and permeability coefficients of films made from PEBA polymers vary due to their different chemical structure. Table 1 shows the chemical compositions and physical properties of some PEBA polymers. Among these polymers, the selectivity of

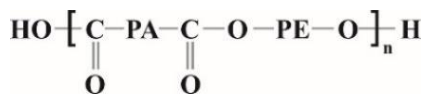


Figure 1. Chemical arrangement of PEBA polymers [7]

TABLE 1. Chemical compounds and physical properties of some PEBA polymers [7]

Type Polymer	Content PE (wt%)	Density (g/cm ³)	Melting temperature (°C)
2533	74.8 ,80	1.01	137, 126
3566	72.9 ,70	1.01	155, 142
4033	44,47	1.01	18, 159
5533	37.8	1.01	160
6333	42.2	-	170
1047	45	1.09	156
4011	43	1.14	201
1657	60	1.14	204

grade 1657 for CO₂ separation was the highest [12]. Zeolites have regular and tiny and controllable pores. They can act as a molecular sieve in the polymer membrane body [13]. Type A zeolite is a known synthetic example of the common compound NaI. [AlO₂.SiO₂]12.27H₂O [14].

This type of zeolite has three different groups, 4A, 3A, and 5A, which differ in the type of cations present in their internal structure [15,16].

Often, zeolite type 4A (Figure 2) is used to absorb water and hazardous gases. But due to its pore size, it can play an essential role as a CO₂ molecule sifting [17,18]. These excellent properties help us to commercialize this nanocomposite. In Table 2, a summary of carbon dioxide separation research by nanocomposite membrane is compiled.

The objective of this research is to solve the weaknesses in permeability and selectivity which gained a suitable position in the Robeson diagram. As mentioned in the introduction, the Robson diagram is presented as an indicator for the commercialization of membranes, so the data were marked on the Robson diagram, and in this way, the evaluation of the commercialization of the nanocomposite membrane was done.

2. EXPERIMENTAL

2. 1. Materials Required For Membrane Preparation

Pebax1657 was selected, made by French Arkema company with a density of 1.14 g/cm³. Zeolite 4A powder made by Behdash Chemical Company of Iran was prepared. This material has a bulk density of 0.5 g/cm³ and an average particle size of 250 to 500 nm. DMF solvent with a purity of 99% was sealed from Neutron Iran and standard hexane solvent was purchased from Merck (Darmstadt, Germany). Gases O₂, N₂, CH₄, and CO₂ with a purity of 99.9% were bought and used from Khorramshahr gas oxygen company.

2. 2. Devices Used In Membrane Preparation and Analysis

XRD analysis with XRD Philips pw1730 device, FE-SEM analysis with TESCAN MIRA3 device, FT-IR analysis with Thermo company model AVATAR. T hedevice, BET analysis with particular surface

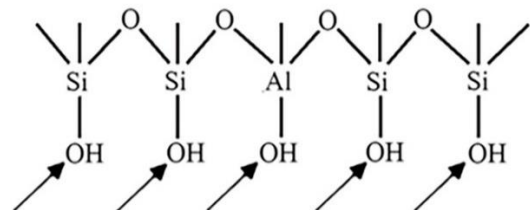


Figure 2. 4A zeolite structure [17]

TABLE 2. A selection of past research on membrane preparation with Pebax polymer and different nanoparticles

Ref.	Filler	Polymer	P _{CO2}	Selectivity
[24]	Zn/Co-ZIF	Pebax1657	102.5	16.4
[25]	Zeolite 13X	Pebax1657	168.59	45
[26]	ZIF-8	Pebax1074	144	72
[27]	ZnO	Pebax1074	152.27	13.52
[28]	TiO ₂	Pebax1657	172	24.8
[29]	ZIF8	Pebax2533	727	63
[30]	Al ₂ O ₃	Pebax1657	159.27	24.73
[31]	ZIF-8	Pebax1657/PE	758	16.1
[32]	DD3R	Pebax1074	188	38.5
[33]	ZIF-7	Pebax1657	150	40
[34]	NH ₂ -CuBTC	Pebax1657	163	26.2
[35]	ZIF-7	Pebax1657	145	23
[36]	Zeolite NaY	Pebax1657	131.8	130.8
[37]	Zeolite NaX	Pebax1657/PES	45	121.5
[38]	ZIF-8	Pebax2533	1293	9
This work	4A	Pebax1657	115.5	CO ₂ /CH ₄ 32.3
This work	4A	Pebax1657	135.5	CO ₂ /O ₂ 20.53
This work	4A	Pebax1657	166.1	CO ₂ /N ₂ 75.19

measuring device: Belsorp mini II from Micro teach Bel Corp, Japan.

TGA/DSC analysis was done by TA company model Q600 device made in USA. To perform the mechanical resistance test was used Tensile Zwick device made in England, model CAT-350-56. The ultrasonic bath machine was manufactured by backer company vCLEAN1-L2. The thickness of the samples was measured by a digital thickness model GT-313-A1 made in Japan.

2. 3. Membrane Preparation And Synthesis Steps

Researchers have selected the membrane's thickness range between 60 and 120 μm [19-21]. Based on this, the amount of materials needed to prepare the membrane was roughly estimated according to the diameter of the petri dish and the thickness of 100 μm . Finally, after synthesizing the membranes, their thickness was measured using a thickness gauge. The nanocomposite was prepared by the solution mixing method.

To reach a concentration of 2.5 wt% of zeolite in the membrane, the first, 0.011 g of zeolite powder was placed

at 70°C for 4 hours. In this way, the moisture was removed from the zeolite [22]. Then 12.076 g of DMF solvent (96.5% Wt. membrane) was added and placed on a magnetic stirrer at a temperature of 55°C for 4 hours [23].

The solution was placed in an ultrasonic bath for 15 minutes. In this way, we ensure the uniform distribution of nanoparticles and the removal of bubbles in the solution. This bath was set at a temperature of 50 °C, a frequency of 42 kHz, and a power of 50 W.

At this stage, the amount of 0.427 g of Pebax1657 granules was added to the solution and it was placed in an oil, and reflux bath at a temperature of 140 °C for 4 hours. To preserve the morphology of the nanocomposite and prevent damage to its structure, the bath was turned off 3 minutes before casting. In this way, the polymer was slightly cooled and ready for casting. Also, the glass petri dish was heated to 80 °C in the oven.

Then the obtained nanocomposite solution was poured into a Petri dish and immediately placed in the oven. The drying temperature and time were set at 40°C and 40 hours. During this time, the membrane was dehydrated. The Petri dish containing the membrane was removed from the oven, and a few drops of standard hexane solvent were poured on its surface.

So that its surface is free of any dust and undesirable particles. Then, for better drying and to ensure complete evaporation of the solvent, the petri dish containing the membrane was placed in a vacuum oven. The temperature of the oven was set at 45 °C. After 4 hours, the membrane was easily separated from the Petri dish and was ready for the permeability test.

In the same way, zeolite was made in the membrane for concentrations of 5, 8, 11.5, 16, and 22% Wt. The nanocomposite membranes prepared in this research were named Pebax1657/4A. Their thickness was measured and coded according to Table 3.

2. 4. Measurement of Permeability and Selectivity

The gas permeability measurement system was designed and built as a constant volume and according to Figure 3.

TABLE 3. Combination of polymer and nanoparticle in nanocomposite membranes

No	Pebax %Wt.	4A Zeolite wt%	ID
1	100	0	PA-0
2	97.5	2.5	PA-2.5
3	95	5	PA-5
4	92	8	PA-8
5	88.5	11.5	PA-11.5
6	84	16	PA-16
7	78	22	PA-22

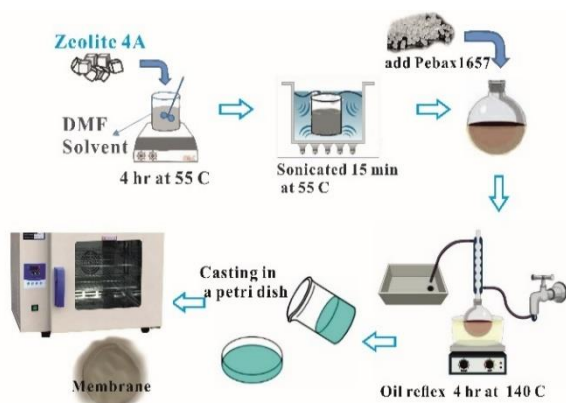


Figure 3. Nanocomposite membrane synthesis steps

This system can calculate gas permeability at different pressures and temperatures. The membrane cell is made of pure steel metal. To prevent gas leakage, rubber rings were installed on both sides of the membrane. The effective area of the membrane in this system is 17.71 cm².

Permeability experiments were performed at temperatures of 25, 35, 50, and 75 °C and pressures of 2, 5, 8 and 12 bars, each with three repetitions. Gas permeability was calculated using Equation (1) and reported in the Barrer unit.

$$P_{(\text{Barrer})} = \frac{273.15 \times 10^{10} LV dP}{760 \times 76 (AT - \frac{P_0}{14.7}) dt} \quad (1)$$

1 Barrer = 10⁻¹⁰ cm³ (STP)·cm / (cm²·s·cmHg)

In Equation (1), V (cm³) is the volume of the reservoir after the cell, L (cm) is the thickness of the membrane, A (cm²) is the effective area of the membrane, T (K) is the temperature, (psia) P₀ is the absolute pressure of the inlet gas and (bar/s) dP/dt is the pressure variation with time [39,40].

The selectivity of ideal gases was calculated using the equation 2 [41,42]. P_A and P_B are the permeability of gases A and B, respectively. The selectivity test results are discussed in the next sections; the selectivity expressed as ratio of P_A and P_B.

$$\alpha_{A/B} = \frac{P_A}{P_B} \quad (2)$$

Experimental set up for the gas permeability measurements is shown in Figure 4.

3. RESULTS AND DISCUSSION

3.1. Analysis of X-ray Diffraction (XRD) XRD analysis was used to investigate the crystal structure of the synthesized membrane.

This analysis was performed from 10° to 80° with a step of 0.05° per second. The results of this analysis are shown in Figure 5. The zeolite phase is formed and has a

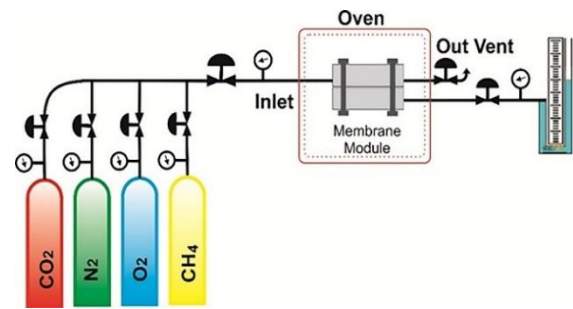


Figure 4. Permeability measurement system

crystal structure and favorable purity. The primary and significant peaks of the following particles after modification are related to X-ray reflection from planes 12.49, 20.09, 22, 27, 30, and 34 in the crystal structure of nanoparticles.

By comparing these figures with the results reported by other researchers [43], it can be said that the changes in the membrane structure are related to the addition of zeolite. In general, modifying the surface with non-crystalline agents reduces the crystallinity of the base particles. In this study, the size of the peaks in the central angles increased, which indicates an increase in membrane crystallinity and an increase in mechanical strength.

3.2. Infrared Fourier Transforms (FT-IR) This analysis was performed on membranes from 600 cm⁻¹ to 4000 cm⁻¹. As shown in Figure 6, the prominent peaks of pure Pebax1657 membrane around 1089 cm⁻¹ wave number were attributed to stretching vibration (C-O-C) of ether group in soft parts. The height at 1635 cm⁻¹ is the stretching vibrations of (O=C) carbonyl in (H-N-O=C). The rise in the wave number of 1729 cm⁻¹ was attributed to another carbonyl group (C=O-O), both of which are in the complex phase.

The peak at 1538 cm⁻¹ is related to N-H bending vibration in polyamide parts and the peak at 3292 cm⁻¹ is related to stretching vibration (N-H). Also, the elevation of 2861 cm⁻¹ and the peak of 1460 cm⁻¹ was related to C-H stretching and bending vibration, respectively.

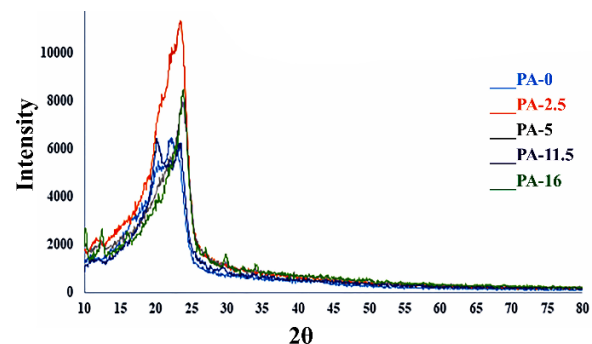


Figure 5. X-ray diffraction (XRD)

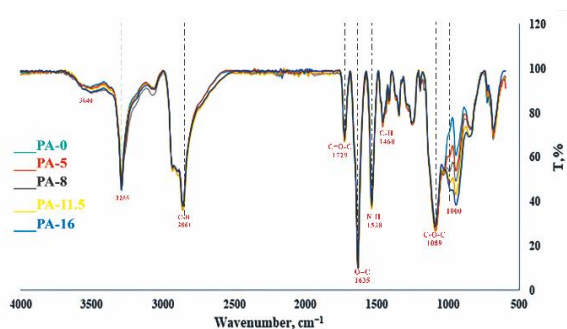


Figure 6. Fourier transform infrared spectroscopy

These results were in good agreement with another research [44]. In the spectrum of zeolite 4A, the broad absorption band in the wave number of 3255 cm^{-1} to 3640 cm^{-1} and the absorption band at 1650 cm^{-1} are related to hydroxyl (-OH) or silanol groups. Absorptions in wave number 1000 cm^{-1} are associated with O-Si or O-Al bending vibrations [45]. As the zeolite loading increased, the corresponding intensity of the peak at 3300 cm^{-1} also increased.

This significant change is attributed to filler phase loading. The absorption bands of zeolite overlap with the related bands in the Pebax spectrum. As the percentage of zeolite increases, the peak becomes higher at 1000 cm^{-1} due to the combined effect of Si-O or Al-O bonds in the zeolite. Finally, it can be said that the functional groups of Pebax and zeolite are placed next to each other with the help of physical bonds, and the formation of chemical bonds is ruled out.

3. 3. Imaging By Method Scanning Electron Microscopy (FE-SEM)

The behavior of polymeric membranes depends on their structure and morphology. Any defect in the membrane structure can cause poor performance in permeability. Therefore, FE-SEM photography was carried out to examine the morphology of the membranes. Figure 7 shows the FE-SEM images of the fabricated membranes.

The pure Pebax membrane (PA-0) has a uniform surface and shows that its preparation method is suitable. According to these images, it can be seen that by adding nano zeolite to the polymer, the morphology of the membrane surface changes.

By increasing the amount of zeolite, the intensity of these changes also increases. Tendency to aggregation and clumping has been observed in the 16% zeolite loading sample. The imaging of the cross-section of the pure Pebax membrane with 8% and 11.5% loading is shown in Figure 7 (G, H and I), respectively; their thicknesses were 82.3, 83.95, and 91.1 μm .

3. 4. X-ray Energy Scattering Spectroscopy (EDAX)

Al, Si, and Na are the main elements of zeolite 4A,

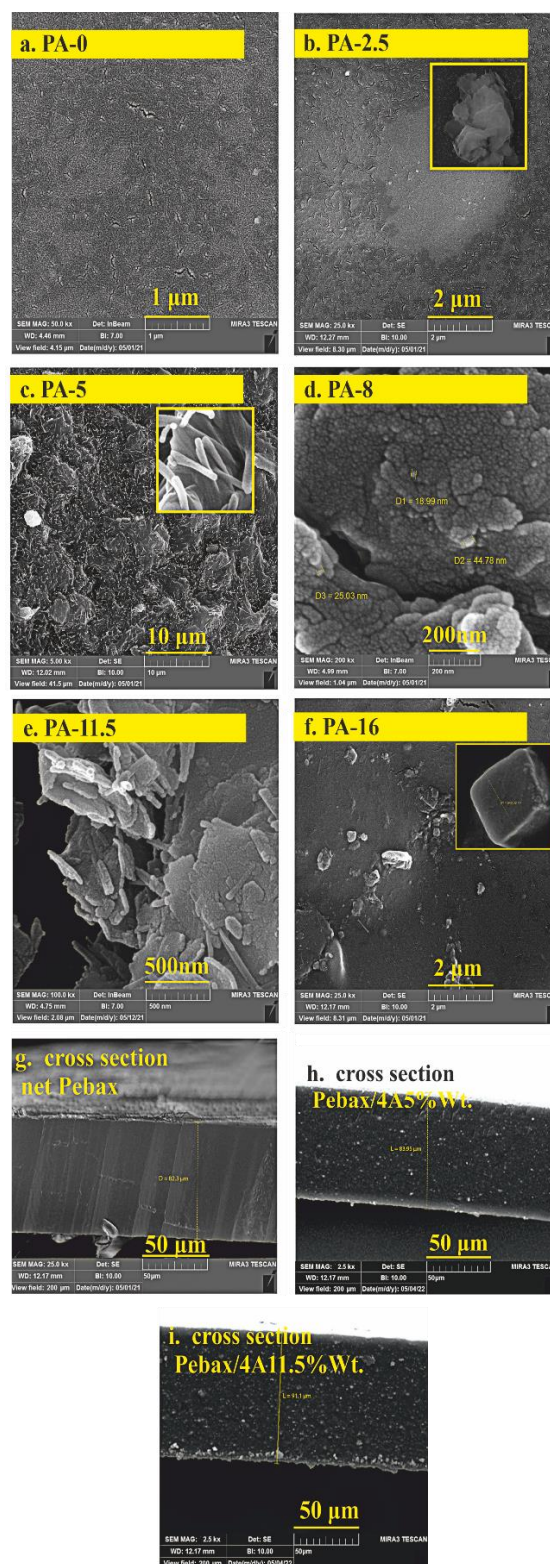


Figure 7. Scanning Electron Microscope (FE-SEM)

making up about 70 Wt.% of its atoms. The results of this analysis, according to Table 4, show that the percentage

of these atoms increases with an increase in the amount of zeolite in the membrane.

Also, Figures 8 and 9 show EDAX images for the the dispersion and proper distribution of elements on the surface of the membrane.

Still, the data of this analysis prove that the constructed membranes overcome this problem and the distribution of particles inside the polymer is uniform and acceptable. If the Si/Al ratio is less than 2, it indicates the hydrophilicity of the membrane [46]. In Table 4, this ratio for the PA-11.5 membrane is about 0.67. Membrane hydrophilicity can be an indicator of better CO₂ selectivity.

3. 5. Surface Measurement Specificity and Porosity (BET)

BET analysis was performed to determine the physical properties of the synthesized

TABLE 4. The percentage of the number of central atoms of zeolite in the samples of the constructed membranes

Na	Si	Al	ID
0.0	0.02	0.02	PA-0
0.11	0.16	0.22	PA-2.5
0.27	0.23	0.34	PA-5
0.47	0.52	0.94	PA-8
0.76	0.48	0.71	PA-11.5
0.82	0.76	1.06	PA-16

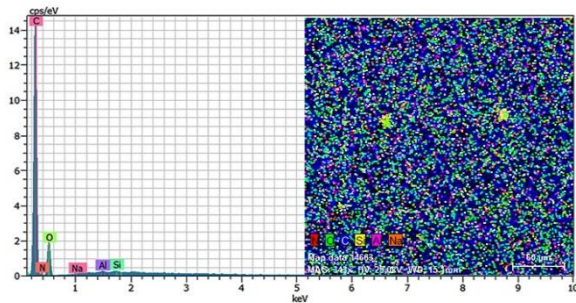


Figure 8. EDAX-Mapping PA-0

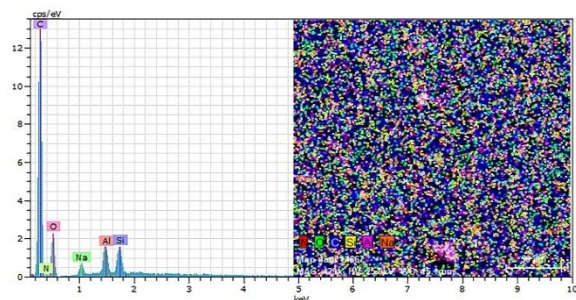


Figure 9. EDAX-Mapping PA-11.5

membranes. In this specific surface area analysis, the total volume of specific pores, the size of the pore diameter and their distribution on the membrane surface were calculated.

Table 5 summarized that after loading nanoparticles, the specific surface area of the membrane increased by 46%. Increasing this parameter affects gas absorption.

Figure 10 shows the absorption-desorption diagram of nitrogen at a temperature of 77 °K of the PA-11.5 membrane. This sample showed the best performance in permeability and selectivity. This diagram is similar to the isotherm of the sixth type of the IUPAC standard. According to this standard, a diameter of less than 2 nm is classified as non-porous.

For a more detailed investigation, the size distribution of the pores on the surface of the membrane was calculated by the BJH method. The results for pore size distribution by BJH method of PA-11.5 membrane is shown in Figure 11. The maximum number of the graph is 1.2nm and 1.8nm, which means that the size of the holes is mostly the same.

3. 6. Thermogravimetric Analysis (TGA)

In this analysis, heating rate of 10 °C/min was applied to the samples. The TGA curves of PA-0 and PA-11.5 membranes were drawn in Figure 12. The noticeable weight loss in the samples up to 206 °C is about 1%, caused by the evaporation of the remaining solvent in the polymer [47].

TABLE 5. BET analysis results

ID	TPV	a _{s, BET}	V _m
PA-0	0.0044627	4.596	1.056
PA-11.5	0.0086457	6.694	1.538

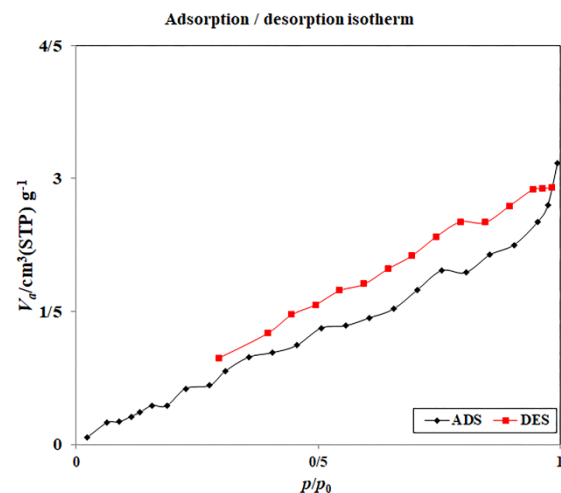


Figure 10. Isothermal absorption and desorption of nitrogen PA-11.5

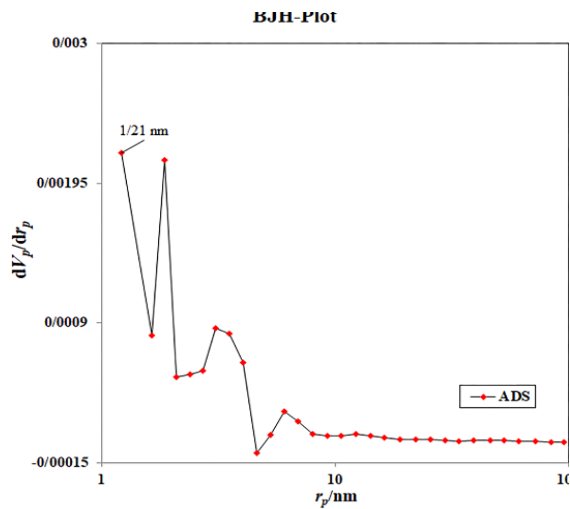


Figure 11. Pore size distribution by BJH method of PA-11.5 membrane

Weight loss in the PA-11.5 membrane started at about 328 °C. The reason is the beginning of the degradation of polymer chains. The DSC diagram shown the amount of energy required for this degradation. From about 361 to 446 °C, all polymer chains were destroyed. From about 450 °C, the polymer started to completely decompose and carbonate. After 525 °C, the weight did not change. But in the PA-0 membrane, the degradation started at 293 °C and at 450 °C, the chains were destroyed.

An increase in the destruction temperature in the nanocomposite membrane compared to the pure membrane is due to the physical bonds between nano zeolite and polymer. These bonds made the membrane strong. The formation of a strong covalent bond between them led to an increase in the energy required for destruction [48].

The DSC diagram shows the energy level needed to overcome these bonds. The TGA curve and the residual weight percentage confirm the presence of nano zeolite in the PA-11.5 membrane structure.

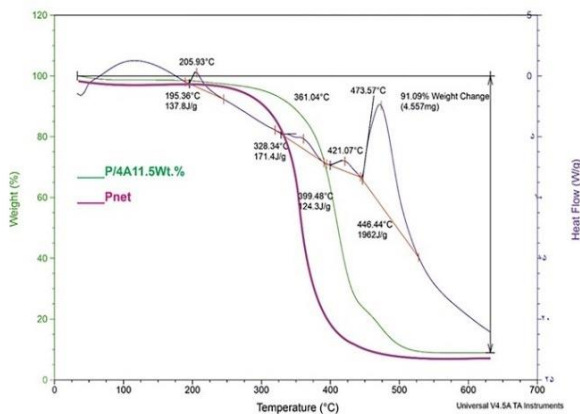


Figure 12. TGA/DSC analysis

3. 7. Analysis of Mechanical Strength

Mechanical strength analysis determines the tensile force a material can withstand before permanent damage. When a material is subjected to tensile force, it will withstand a certain amount of elongation before tearing. In this analysis, it was determined how strong the nanocomposite membrane is compared to the pure membrane.

The strip-shaped samples were placed between these two jaws of the machine and were drawn steadily at a speed of 5 mm/min. In this test, the temperature conditions and stretching rate remained constant. Table 6 shows the reaction of the manufactured membranes during the application of tensile force. In this table, it is shown that by addition of nanoparticles up to 11.5 wt%, the mechanical resistance of the composite membranes increased compared to the pure polymer membrane. The reason for that can be the proper physical bonding of nanoparticles and their coating by a polymer network. Also, this table shows that as the mass of particle increases, the membrane becomes denser. Excellent adhesion between nano zeolite and polymer, as well as their proper distribution on the surface of the membrane, increased the tensile strength.

The results of the EDAX analysis confirm that 4A particles are uniformly distributed in the polymer. The mechanical resistance of PA-16 and PA-22 membranes decreased. These two membranes cannot perform as well as the previous membranes. One of the reasons can be the clumping of nanoparticles in some places because clumping of nanoparticles causes their inability to interact with the polymer matrix and uneven stress distribution [48].

3. 8. Effect of Inlet Pressure

PA-11.5 nanocomposite membrane showed the best performance in permeability tests. For this reason, this membrane was chosen to investigate the effect of feed pressure on permeability and selectivity. By examining Figures 12, 13, and 14, the result of increasing the feed pressure on the permeability and selectivity of the membranes can be observed. As the pressure increased, the permeability of

TABLE 6. The mechanical performance of membranes

Loading Zeolite (Wt%)	Tensile strength (MPa)	Elastic modulus (MPa)	Elongation at break (%)
0	21.8	148.4	791 ± 2
2.5	23.1	135.3	812 ± 5
5	26.7	128.6	641 ± 5
8.5	29.3	118.5	598 ± 3
11.5	34.5	116.1	478 ± 3
16	19.9	95.8	251 ± 5
22.5	12.7	83.2	141 ± 5

CO₂ increased dramatically. at the same time, the permeability of other gases increased less. An increase in CO₂ permeability at higher pressures can be due to an increase in solubility due to the absorption of more CO₂ molecules in the polymer network [49]. Figure 12 demonstrates TGA/DSC analysis of the fabricated membrane

With an increase in pressure, the number of CO₂ molecules on the surface of the membrane increases. This increase creates a hydrogen bond between the O atom corresponding to the CO₂ molecule and the H of the amide groups on the surface of the polymer, for this reason, the selectivity of this gas increases. [6, 50]. Figure 13 shows the Robeson constraint chart for the selectivity of CO₂/CH₄ and CO₂/N₂ for the different Pebax 1657, Pebax 1657/4A and Pebax 1657/4A 11.5wt% of nanoparticles. In Figure 13, the performance of the optimized membrane in this study was marked on the Robeson diagram. This figure shows that the membrane was placed on the Robeson line. As a result, it can be considered a suitable option for separating carbon dioxide gas from other light gases in chemical industries.

3. 9. Effect of Operating Temperature The kinetic energy of gas molecules at high temperatures destroyed some of the polymer chains ,and the polymer network became more flexible. This flexibility in the polymer network can increase the molecular free volume coefficient in the membrane. Therefore, the membrane permeability increased, but the selectivity significantly decreased [51]. The reason for that can be the decrease in the solubility of CO₂ at temperatures higher than 35°C. If the solubility coefficient decreases, the selectivity of CO₂

also decreases compared to other gases [6]. Figure 14 shows CO₂ / N₂ selectivity at different temperatures and pressures; while Figure 15 illustrates CO₂ / CH₄ selectivity at different temperatures and pressures. In addition, the selectivity of CO₂/O₂ at different temperatures and pressures is shown in Figure 16.

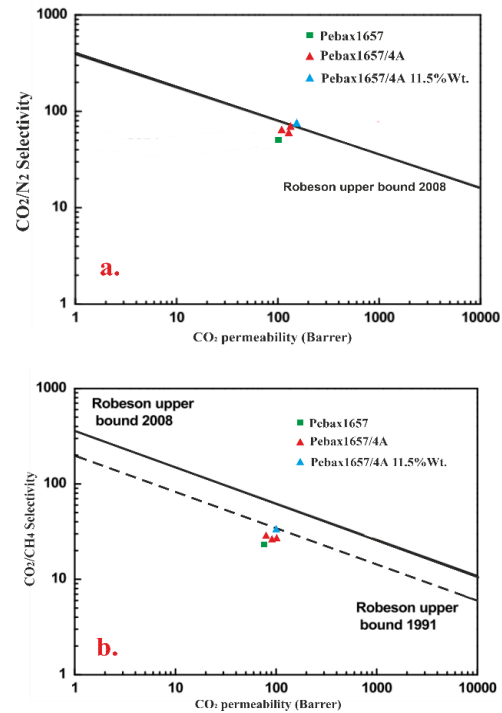


Figure 13. Robeson constraint chart

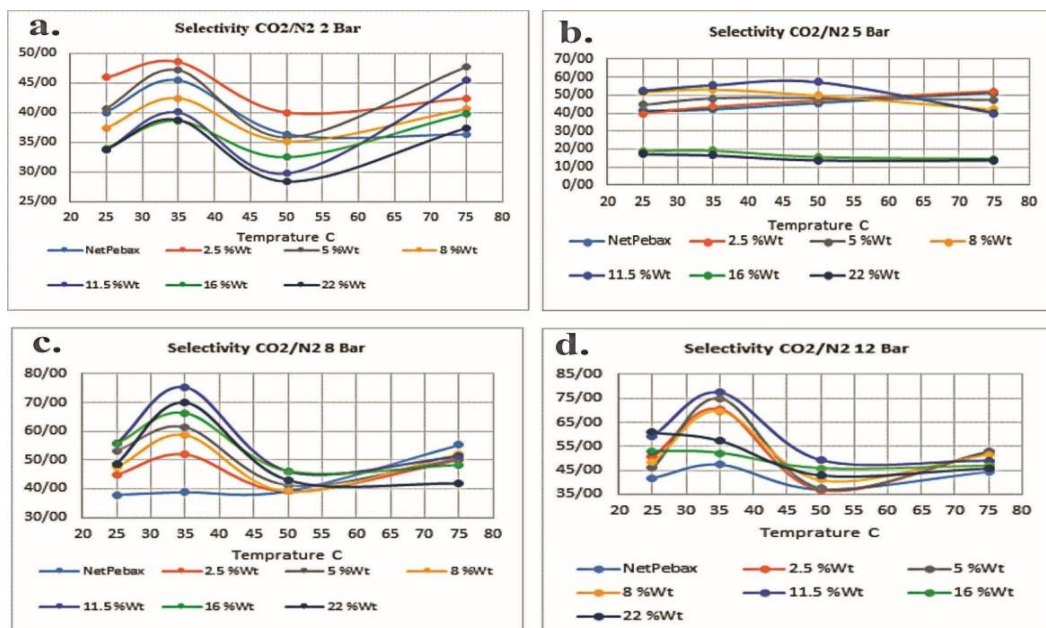


Figure 14. CO₂ / N₂ selectivity in different temperatures and pressures

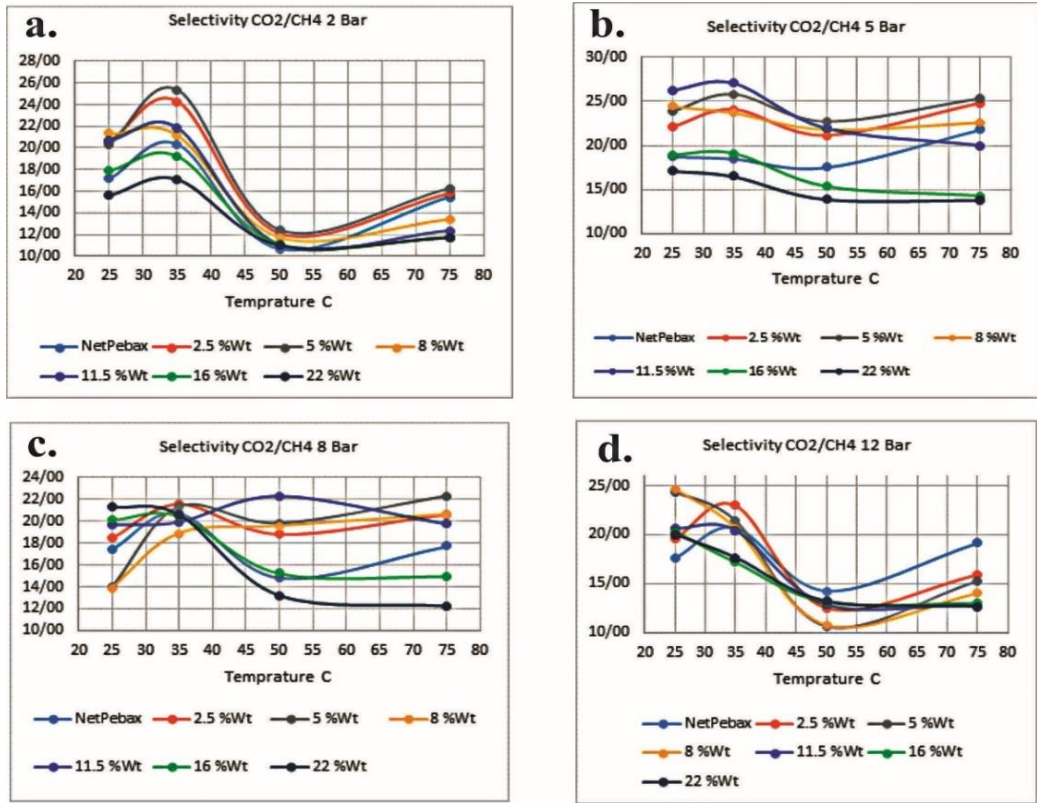


Figure 15. CO₂ / CH₄ selectivity in different temperatures and pressures

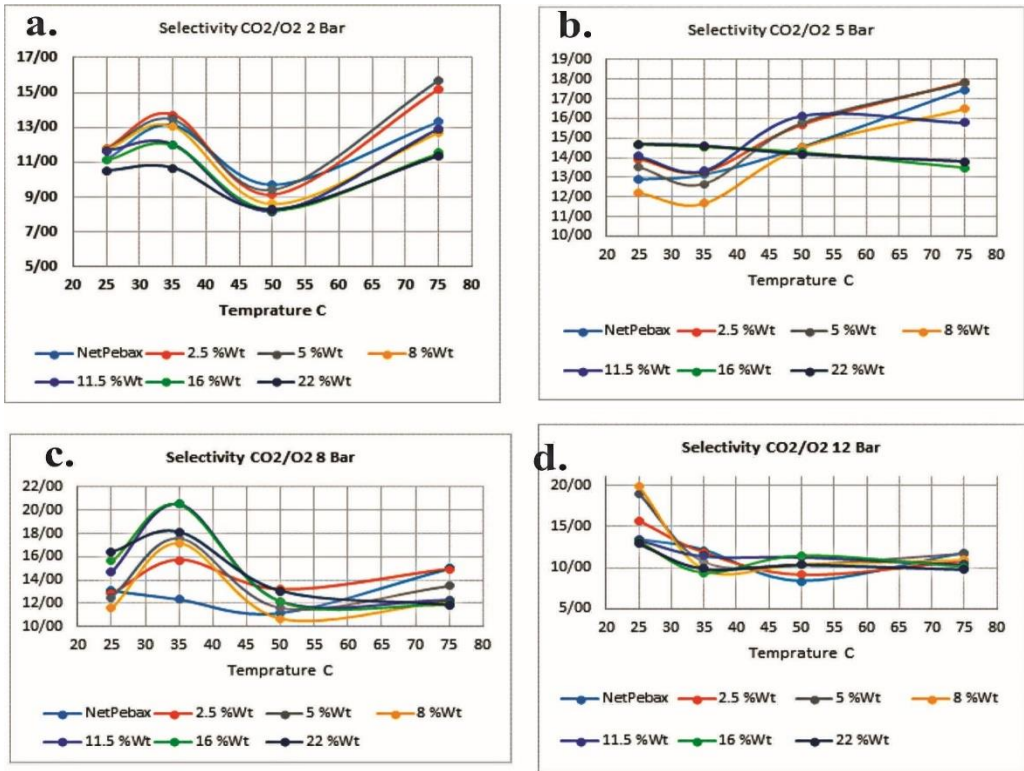


Figure 16. CO₂/ O₂ selectivity in different temperatures and pressures

4. CONCLUSION

In this research, Pebax 1657/4A zeolite nanocomposite membranes were prepared by casting and solvent evaporation. Their performance was investigated under operating conditions of 25 to 75 °C and pressures of 2 to 12 Bar for separating CO₂ gas relative to N₂, CH₄, and O₂. The results of FT-IR test denied the formation of a chemical bond between zeolite and polymer. FE-SEM images and EDAX analysis showed that the nano zeolites were well dispersed in the polymer, and a suitable nanocomposite membrane structure was obtained.

The TGA/DSC test showed that the thermal resistance of the nanocomposite membrane has increased compared to the polymer membrane. It also proved physical solid bonds between nano zeolite and polymer. CO₂ selectivity increased with increasing operating pressure. An increase in the operating temperature causes a significant increase in the permeability of gases due to an increase in their molecular kinetic energy and the polymer chains becoming more flexible. But the selectivity was significantly reduced. BET test showed that the pore size of nanocomposite membranes is less than 2 nm. This size is proportional to CO₂ molecules. These molecules can pass with less resistance than the pure polymeric membrane. Nanoparticle loading reduces the density of polymer chains and weakens the hydrogen bond between them. This factor increases the free volume between molecules and increases permeability.

The results of the gas permeability test showed that the best result was obtained at a temperature of 35 °C by adding 11.5% Wt. of zeolite to the polymer membrane. The best selectivity of CO₂ against N₂, O₂, and CH₄ was obtained at 12, 8, and 5 bar pressures, respectively.

Finally, the selectivity of the Pebax1657/4A nanocomposite membrane was 64, 67, and 45% better than pure Pebax in the mentioned operating conditions, respectively. As mentioned in the introduction, Robeson presented a limit in the permeability selectivity diagram, which was called Robeson's upper limit. The closer the polymer membrane is to this upper limit of the graph, the more suitable it is for industrialization.

Nowadays, the elimination of these gases has become a vital issue for researchers so that they can prevent the excessive heating of the earth.

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Persian Abstract

چکیده

جداسازی دی اکسید کربن برای محیط زیست ضروری است. استفاده از غشاهای برای جداسازی این گاز مقرون به صرفه است، اما ضعف در نفوذپذیری و استحکام مکانیکی مانع تجاری سازی آنها شده است. رابسون ثابت کرد که نفوذپذیری و گزینش پذیری رابطه معکوس دارند و حد بالایی برای جفت گازها ارائه کرد. وی اظهار داشت که هر غشایی که بالاتر از این حد قرار گیرد، قابل تجاری سازی است. دانشمندان برای غلبه بر این مشکل غشاهای ماتریس مخلوط را پیشنهاد کردند. این غشاهای شامل دو فاز پلیمری و معدنی هستند. هدف از این تحقیق رفع نقاط ضعف ذکر شده و کسب جایگاه مناسب در نمودار رابسون می باشد. پلیمر Pebax و زئولیت 4A به ترتیب به عنوان فازهای پلیمری و معدنی برای ساخت غشا انتخاب شدند. غشاهای ساخته شده توسط تست های XRD، FT-IR، FE-SEM، BET، EDAX، TGA/DSC و استحکام مکانیکی مورد ارزیابی قرار گرفتند. در نهایت، گزینش پذیری دی اکسید کربن در مقایسه با نیتروژن، اکسیژن و متان به ترتیب ۵۳، ۶۷ و ۷۵ درصد بهبود یافت و موقعیت خوبی در نمودار رابسون به دست آورد.
